

Compensation of Multi-Sinusoidal Disturbance for Linear Plant with Input Delay

Oleg I. Borisov

Research Supervisor: Anton A. Pyrkin

ITMO University

Traditional School for Young Scientists VI
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Plant Model

Consider the linear plant

$$\dot{x}(t) = Ax(t) + Bu(t - D) + B\delta(t), \quad (1)$$

$$y(t) = Cx(t) + \alpha\delta(t), \quad (2)$$

where $x \in \mathbb{R}^n$ is unknown, $y(t)$ is measurable, $u(t)$ has initial condition $u(t - D) = 0$ for $t < D$, $D \geq 0$ is known constant delay, A , B , C are corresponding matrices, $\alpha \neq 0$.

The input disturbance $\delta(t)$ has a view

$$\delta(t) = \sigma + \sum_{i=1}^k [\mu_i \sin(\omega_i t) + \nu_i \cos(\omega_i t)]. \quad (3)$$

Purpose of Control

The objective is to find the control $u(t)$ that achieves regulation of the state variables

$$\lim_{t \rightarrow \infty} x(t) = 0, \quad (4)$$

under the following assumptions

Assumption 1. A , B , C , and α are known.

Assumption 2. (A, B, C) is a completely controllable and observable triple.

Assumption 3. A lower bound on the disturbance frequencies is known.

Frequency Estimation

Consider the linear observer

$$\dot{\hat{x}}_1(t) = A\hat{x}_1(t) + Bu(t - D) + L\tilde{y}_1(t), \quad (5)$$

$$\hat{y}_1(t) = C\hat{x}_1(t). \quad (6)$$

Then the observer error is given by

$$\tilde{x}_1(t) = x(t) - \hat{x}_1(t), \quad (7)$$

$$\dot{\tilde{x}}_1(t) = (A - LC)\tilde{x}_1(t) + B\delta(t) - L\alpha\delta(t), \quad (8)$$

$$\tilde{y}_1(t) = y(t) - \hat{y}(t) = C\tilde{x}_1(t) + \alpha\delta(t). \quad (9)$$

Use the function $\tilde{y}_1(t)$ as information carrier about the disturbance. Write it in the following form

$$\tilde{y}_1(t) = \bar{\sigma} + \bar{\varepsilon}(t) + \sum_{i=1}^k [\bar{\mu}_i \sin(\omega_i t) + \bar{\nu}_i \cos(\omega_i t)]. \quad (10)$$

Multi-Sinusoidal Signal Model

It is known that the signal $\tilde{y}_1(t)$ can be generated by the following differential equation

$$p(p^2 - \theta_1)(p^2 - \theta_2) \dots (p^2 - \theta_k) \tilde{y}_1(t) = 0, \quad (11)$$

where $\theta_i = -\omega_i$, $i = 1, \dots, k$ are constant parameters.

Rewrite (11) using the Laplace transformation

$$s^{2k+1} \tilde{y}_1(s) = \bar{\theta}_1 s^{2k-1} \tilde{y}_1(s) + \dots + \bar{\theta}_k s \tilde{y}_1(s) + d(s), \quad (12)$$

where $d(s)$ denotes initial conditions caused by the function $\varepsilon_1(t)$ and the parameters $\bar{\theta}_i$, $i = 1, \dots, k$ can be calculated by the following system

$$\begin{cases} \bar{\theta}_1 = \theta_1 + \theta_2 + \dots + \theta_k, \\ \bar{\theta}_2 = -\theta_1\theta_2 - \theta_1\theta_3 - \dots - \theta_{k-1}\theta_k, \\ \vdots \\ \bar{\theta}_k = (-1)^{k+1} \theta_1\theta_2 \dots \theta_k. \end{cases} \quad (13)$$

Regression Model

Introduce the linear filter

$$\xi(s) = \frac{\lambda_0^{2k}}{\gamma(s)} \tilde{y}_1(s), \quad (14)$$

where $\lambda_0 > 0$, $\gamma(s) = s^{2k} + \gamma_{2k-1}s^{2k-1} + \dots + \gamma_1s + \gamma_0$ is a Hurwitz polynomial with $2k$ different eigenvalues $\lambda_j, j = 1, \dots, 2k$. Let $\gamma_0 = \lambda_0^{2k}$ and $\lambda = \min_{j=1, \dots, 2k} \{|\operatorname{Re} \lambda_j|\}$.

Multiplying (12) by $\frac{\lambda_0^{2k}}{\gamma(s)}$ with (14) we obtain

$$s^{2k+1}\xi(s) = \bar{\theta}_1 s^{2k-1}\xi(s) + \dots + \bar{\theta}_k s \xi(s) + \frac{\lambda_0^{2k}}{\gamma(s)} d(s). \quad (15)$$

After the inverse Laplace transformation for the filter (14) and the input signal (10) we get the relation

$$\xi^{(2k+1)}(t) = \Omega^T(t) \bar{\Theta} + \varepsilon(t) \quad (16)$$

where $\Omega^T(t) = [\xi^{(2k-1)}(t) \quad \dots \quad \xi^{(3)}(t) \quad \xi^{(1)}(t)]$ is a regressor of functions $\xi^{(j)}(t)$, $\bar{\Theta}^T = [\bar{\theta}_1 \quad \dots \quad \bar{\theta}_{k-1} \quad \bar{\theta}_k]$ is a vector of unknown parameters depending on frequencies.

Adaptive Frequency Estimation Scheme

The update law

$$\hat{\omega}_i = \sqrt{|\hat{\theta}_i|}, \quad (17)$$

where estimates θ_i calculated using $\hat{\theta}_i$ that are elements of a vector $\hat{\Theta}$:

$$\dot{\hat{\Theta}} = \Upsilon(t) + K\Omega(t)\xi^{(2k)}(t), \quad (18)$$

$$\dot{\Upsilon}(t) = -K\Omega(t)\Omega^T(t)\hat{\Theta}(t) - K\dot{\Omega}(t)\xi^{(2k)}(t). \quad (19)$$

where $K = \text{diag}\{k_i > 0, i = \overline{1, k}\}$, guarantees that the estimation error $\tilde{\omega}_i = \omega_i - \hat{\omega}_i$ exponentially converges to zero:

$$|\tilde{\omega}_i(t)| \leq \rho_1 e^{-\beta_1 t}, \quad \rho_1, \beta_1 > 0, \quad \forall t \geq 0. \quad (20)$$

Harmonics Extracting

Write the linear filter $\xi(t)$ as follows

$$\xi(t) = \left[\frac{\lambda_0}{\gamma(p)} \right] \tilde{y}_1(t) = \left[\frac{\lambda_0}{\gamma(p)} \right] \left(\left[\frac{b(p)}{a(p)} \right] \delta(t) + \bar{\varepsilon}(t) \right) = \xi_0 + \varepsilon_2(t) + \sum_{i=1}^k \xi_i(t), \quad (21)$$

where

$$\xi_0 = \sigma \frac{b_0}{a_0}, \quad (22)$$

$$\begin{aligned} \xi_i(t) &= M_i \mu_i \sin(\omega_i t + \varphi_i) + M_i \nu_i \cos(\omega_i t + \varphi_i) \\ &= \begin{bmatrix} \mu_i & \nu_i \end{bmatrix} \begin{bmatrix} M_i \sin(\omega_i t + \varphi_i) \\ M_i \cos(\omega_i t + \varphi_i) \end{bmatrix} = \begin{bmatrix} \mu_i & \nu_i \end{bmatrix} \varsigma_i \end{aligned} \quad (23)$$

$$M_i = \left| \frac{\lambda_0}{\gamma(j\omega_i)} \frac{b(j\omega_i)}{a(j\omega_i)} \right|, \varphi_i = \arg \left(\frac{\lambda_0}{\gamma(j\omega_i)} \frac{b(j\omega_i)}{a(j\omega_i)} \right). \quad (24)$$

For the variable $\xi(t)$ we have

$$\xi(t) = \xi_0 + \xi_1(t) + \xi_2(t) + \dots + \xi_k(t). \quad (25)$$

We get the realizable estimation scheme for variables ξ_0 and $\xi_i(t)$:

$$\begin{bmatrix} \hat{\xi}_1(t) \\ \hat{\xi}_2(t) \\ \vdots \\ \hat{\xi}_k(t) \end{bmatrix} = \begin{bmatrix} \hat{\theta}_1 & \dots & \hat{\theta}_k \\ \hat{\theta}_1^2 & \dots & \hat{\theta}_k^2 \\ \vdots & \ddots & \vdots \\ \hat{\theta}_1^k & \dots & \hat{\theta}_k^k \end{bmatrix}^{-1} \begin{bmatrix} \xi^{(2)}(t) \\ \xi^{(4)}(t) \\ \vdots \\ \xi^{(2k)}(t) \end{bmatrix}, \quad \hat{\xi}_0(t) = \xi(t) - \sum_{i=1}^k \hat{\xi}_i(t). \quad (26)$$

Amplitudes and Bias Identification

The bias can be found as follows

$$\hat{\sigma} = \frac{a_0}{b_0} \hat{\xi}_0. \quad (27)$$

Introducing the auxiliary function of time $\hat{\Delta}(t) = \sum_{i=0}^k \sin(\hat{\omega}_i t)$ consider the auxiliary filter

$$\vartheta(t) = \left[\frac{\lambda_0}{\gamma(p)} \frac{b(p)}{a(p)} \right] \hat{\Delta}(t) = \sum_{i=1}^k \vartheta_i(t) + \varepsilon_3(t). \quad (28)$$

The signals $\vartheta_i(t)$ and its derivatives equal

$$\vartheta_i(t) = M_i \sin(\omega_i t + \varphi_i), \quad \dot{\vartheta}_i(t) = \omega_i M_i \cos(\omega_i t + \varphi_i). \quad (29)$$

Using the algorithm of harmonic extraction design the observer for all components of regressors c_i

$$\begin{bmatrix} \hat{\vartheta}_1(t) \\ \hat{\vartheta}_2(t) \\ \vdots \\ \hat{\vartheta}_k(t) \end{bmatrix} = \begin{bmatrix} \hat{\theta}_1 & \cdots & \hat{\theta}_k \\ \hat{\theta}_1^2 & \cdots & \hat{\theta}_k^2 \\ \vdots & \ddots & \vdots \\ \hat{\theta}_1^k & \cdots & \hat{\theta}_k^k \end{bmatrix}^{-1} \begin{bmatrix} \vartheta^{(2)}(t) \\ \vartheta^{(4)}(t) \\ \vdots \\ \vartheta^{(2k)}(t) \end{bmatrix}, \quad (30)$$

$$\begin{bmatrix} \hat{\vartheta}_1(t) \\ \hat{\vartheta}_2(t) \\ \vdots \\ \hat{\vartheta}_k(t) \end{bmatrix} = \begin{bmatrix} 1 & \cdots & 1 \\ \hat{\theta}_1 & \cdots & \hat{\theta}_k \\ \vdots & \ddots & \vdots \\ \hat{\theta}_1^{k-1} & \cdots & \hat{\theta}_k^{k-1} \end{bmatrix}^{-1} \begin{bmatrix} \vartheta^{(1)}(t) \\ \vartheta^{(3)}(t) \\ \vdots \\ \vartheta^{(2k-1)}(t) \end{bmatrix}. \quad (31)$$

Amplitudes and Bias Identification

So we get the algorithm to calculate the regressor functions $\varsigma_i(t)$

$$\hat{\varsigma}_i^T(t) = \begin{bmatrix} \hat{\vartheta}_i(t) & \frac{\hat{\vartheta}_i(t)}{\eta_i(t)} \end{bmatrix}, \quad (32)$$

$$\eta_i(t) = \begin{cases} \hat{\omega}_i(t), & \text{if } \hat{\omega}_i \geq \omega_0, \\ \omega_0, & \text{otherwise,} \end{cases} \quad (33)$$

Eventually, we design the update laws for μ_i and ν_i by the standard approach basing on the regressor model (23)

$$\dot{\hat{\mu}}_i(t) = k_\mu \hat{\vartheta}_i(t) \left(\hat{\xi}_i(t) - \hat{\mu}_i(t) \hat{\vartheta}_i(t) - \hat{\nu}_i(t) \frac{\hat{\vartheta}_i(t)}{\eta_i(t)} \right), \quad (34)$$

$$\dot{\hat{\nu}}_i(t) = k_\nu \frac{\hat{\vartheta}_i(t)}{\eta_i(t)} \left(\hat{\xi}_i(t) - \hat{\mu}_i(t) \hat{\vartheta}_i(t) - \hat{\nu}_i(t) \frac{\hat{\vartheta}_i(t)}{\eta_i(t)} \right), \quad (35)$$

where $k_\mu, k_\nu > 0$ and $\eta_i(t)$ is defined above in (33).

Resultant Disturbance Observer

Using $\hat{\sigma}$, $\hat{\mu}_i$ и $\hat{\nu}_i$ it is easy to obtain disturbance observer $\delta(t)$

$$\hat{\delta}(t) = \hat{\sigma} + \sum_{i=1}^k [\hat{\mu}_i \sin(\hat{\omega}_i t) + \hat{\nu}_i \cos(\hat{\omega}_i t)]. \quad (36)$$

The second observer taking into account the known delay D we can get as follows

$$\begin{aligned} \hat{\delta}(t + D) &= \hat{\sigma} + \sum_{i=1}^k [\hat{\mu}_i \sin(\hat{\omega}_i(t + D)) + \hat{\nu}_i \cos(\hat{\omega}_i(t + D))] \\ &= \hat{\sigma} + \sum_{i=1}^k [\kappa_i \sin(\hat{\omega}_i t) + \zeta_i \cos(\hat{\omega}_i t)], \end{aligned} \quad (37)$$

where

$$\kappa_i = \hat{\mu}_i \cos(\hat{\omega}_i D) - \hat{\nu}_i \sin(\hat{\omega}_i D), \quad (38)$$

$$\zeta_i = \hat{\mu}_i \sin(\hat{\omega}_i D) + \hat{\nu}_i \cos(\hat{\omega}_i D). \quad (39)$$

Control Design

The feedback will be chosen in the form

$$u(t) = -\hat{\delta}(t + D) + \psi(t). \quad (40)$$

Substituting (40) into (1) yields

$$\dot{x}(t) = Ax(t) + B\psi(t - D) + B\tilde{\delta}_1(t). \quad (41)$$

Basing on (41) we introduce the second observer for state variables.

$$\dot{\hat{x}}_2(t) = A\hat{x}_2 + B\psi(t - D) + L\tilde{y}_2(t), \quad (42)$$

$$\hat{y}_2(t) = C\hat{x}_2(t) + \alpha\hat{\delta}(t), \quad (43)$$

Consider a model of the observer error $\tilde{x}_2(t) = x(t) - \hat{x}(t)$ with respect to (1), (2), (42), (43)

$$\dot{\tilde{x}}_2(t) = (A - LC)\tilde{x}_2(t) + B\tilde{\delta}_1(t) - L\alpha\tilde{\delta}_2(t), \quad (44)$$

$$\tilde{y}_2(t) = C\tilde{x}_2(t) + \alpha\tilde{\delta}_2(t). \quad (45)$$

Control Design

Consider model of the delay by the transport PDE (M. Krstic approach)

$$\Psi_t(z, t) = \Psi_z(z, t), \quad 0 < z < D \quad (46)$$

$$\Psi(D, t) = \psi(t) \quad (47)$$

with the initial condition $\Psi(z, 0) = \psi(z - D)$. The solution of this PDE is $\Psi(z, t) = \psi(t + z - D)$, and therefore $\Psi(0, t) = \psi(t - D)$ gives the delayed input. We can now rewrite (41) in the form

$$\dot{x}(t) = Ax(t) + B\Psi(0, t) + B\tilde{\delta}_1(t). \quad (48)$$

Choose the control law for $\psi(t)$ in the form

$$\psi(t) = Ke^{AD}\hat{x}_2(t) + K \int_0^D e^{A(D-\tau)} B\Psi(\tau, t) d\tau. \quad (49)$$

Numerical Example

Consider the following linear plant

$$\dot{x}(t) = \begin{bmatrix} 0 & 1 \\ 0, 1 & -1 \end{bmatrix} x(t) + \begin{bmatrix} 0 \\ 2 \end{bmatrix} u(t-1) + \begin{bmatrix} 0 \\ 2 \end{bmatrix} \delta(t), \quad (50)$$

$$y(t) = [1 \quad 0] x(t) + \delta(t), \quad (51)$$

where the disturbance signal has a view

$$\delta(t) = 1 + 3 \sin(0,8 t) - \cos(0,8 t). \quad (52)$$

Numerical Example

Introduce the first state observer to extract the information about the disturbance from $y(t)$

$$\dot{\hat{x}}_1(t) = \begin{bmatrix} 0 & 1 \\ 0,1 & -1 \end{bmatrix} \hat{x}_1(t) + \begin{bmatrix} 0 \\ 2 \end{bmatrix} u(t-1) + L(y(t) - \hat{y}_1(t)), \quad (53)$$

$$\hat{y}_1(t) = [1 \quad 0] \hat{x}_1(t), \quad (54)$$

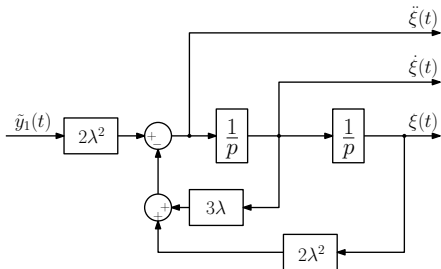
where choose the matrix $L^T = [2 \quad 2]$.

The error signal $\tilde{y}_1(t) = y(t) - \hat{y}_1(t)$ will be used as information carrier about the disturbance.

Introduce the linear filter

$$\xi(t) = \left[\frac{2\lambda^2}{(p^2 + 3\lambda p + 2\lambda^2)} \right] \tilde{y}_1(t), \quad (55)$$

where $\lambda = 1$.



Numerical Example

Write the realizable scheme of frequency identification

$$\hat{\omega}(t) = \sqrt{|\hat{\theta}(t)|}, \quad (56)$$

$$\hat{\theta}(t) = \chi(t) + k\dot{\xi}(t)\ddot{\xi}(t), \quad (57)$$

$$\dot{\chi}(t) = -k\dot{\xi}^2(t)\hat{\theta}(t) - k\ddot{\xi}^2(t), \quad (58)$$

where $k = 2$.

To avoid division by zero introduce the following constraint for the frequency

$$\hat{\omega}(t) = \omega_0, \quad \text{if } \hat{\omega} < \omega_0, \quad (59)$$

where $\omega_0 = 0.5$.

Write the equations for the components of the signal $\xi(t)$

$$\hat{\xi}_1(t) = -\frac{\ddot{\xi}(t)}{\hat{\omega}^2(t)}, \quad \hat{\xi}_0(t) = \xi(t) - \hat{\xi}_1(t). \quad (60)$$

Numerical Example

The bias can be found as

$$\hat{\sigma}(t) = \frac{a_0}{b_0} \hat{\xi}_0(t), \quad (61)$$

where $b_0 = 1.9$ и $a_0 = 3.9$ correspond to the transfer function

$$\frac{b(p)}{a(p)} = C(pI - (A - LC))^{-1}(B - L\alpha) + \alpha = \frac{p^2 + p + 1.9}{p^2 + 3p + 3.9}. \quad (62)$$

Taking into consideration the auxiliary variable $\hat{\Delta}(t) = \sin(\hat{\omega}t)$ consider the filter for $\hat{\Delta}(t)$

$$\hat{\vartheta}(t) = \left[\frac{2(p^2 + p + 1, 9)}{(p^2 + 3p + 2)(p^2 + 3p + 3, 9)} \right] \hat{\Delta}(t). \quad (63)$$

The algorithm for computation of $\hat{\mu}$ and $\hat{\nu}$ looks as follows

$$\dot{\hat{\mu}}(t) = k_\mu \hat{\vartheta}(t) \left(\hat{\xi}_1(t) - \hat{\mu}(t)\hat{\vartheta}(t) + \hat{\nu}(t) \frac{\hat{\vartheta}(t)}{\hat{\omega}^2(t)} \right), \quad (64)$$

$$\dot{\hat{\nu}}(t) = -k_\nu \frac{\hat{\vartheta}(t)}{\hat{\omega}^2(t)} \left(\hat{\xi}_1(t) - \hat{\mu}(t)\hat{\vartheta}(t) + \hat{\nu}(t) \frac{\hat{\vartheta}(t)}{\hat{\omega}^2(t)} \right), \quad (65)$$

where $k_\mu = 2$ and $k_\nu = 3$.

Numerical Example

The first disturbance observer (without delay) has the form

$$\hat{\delta}(t) = \hat{\sigma} + \hat{\mu} \sin(\hat{\omega}t) + \hat{\nu} \cos(\hat{\omega}t). \quad (66)$$

The second disturbance observer (with delay) has the form

$$\hat{\delta}(t + D) = \hat{\sigma} + \kappa \sin(\hat{\omega}t) + \zeta \cos(\hat{\omega}t), \quad (67)$$

$$\kappa = \hat{\mu} \cos(\hat{\omega}D) - \hat{\nu} \sin(\hat{\omega}D), \quad (68)$$

$$\zeta = \hat{\mu} \sin(\hat{\omega}D) + \hat{\nu} \cos(\hat{\omega}D). \quad (69)$$

Write the second state observer for main control scheme

$$\dot{\hat{x}}_2(t) = A\hat{x}_2 + B\psi(t - D) + L(y(t) - \hat{y}_2(t)), \quad (70)$$

$$\hat{y}_2(t) = C\hat{x}_2(t) + \alpha\hat{\delta}(t). \quad (71)$$

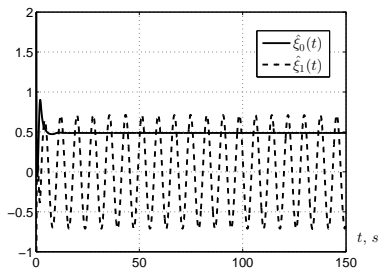
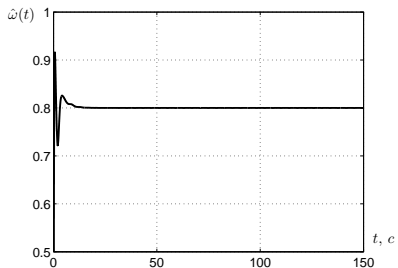
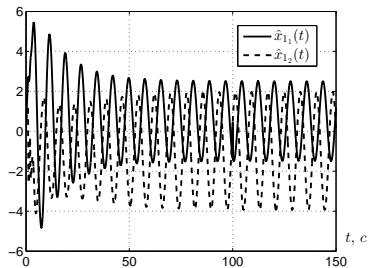
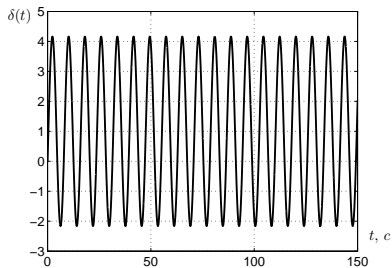
Choose the control signal

$$u(t) = -\hat{\delta}(t + D) + \psi(t), \quad (72)$$

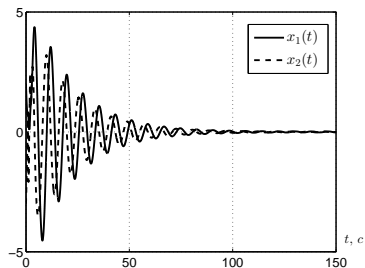
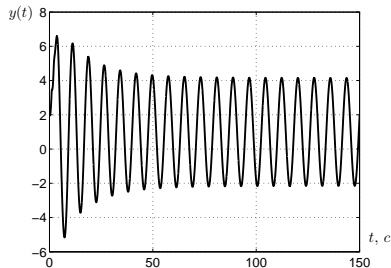
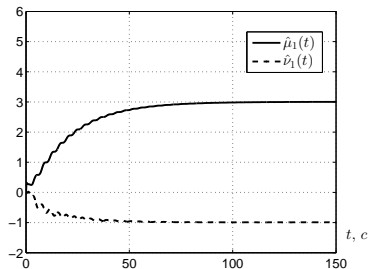
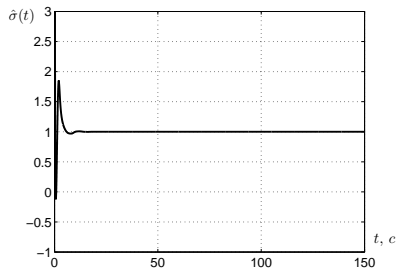
$$\psi(t) = Ke^{AD}\hat{x}_2(t) + K \int_{t-D}^t e^{A(t-z)} B\psi(z) dz, \quad (73)$$

where $K = [2 \quad 2]$.

Numerical Example



Numerical Example



Conclusions

- the adaptive controller for the linear plant with the input delay was designed
- the obtained algorithm cancels the unknown disturbance affecting on the input and the output providing exponentially decaying to zero for the state variables
- the effectiveness of the proposed approach was illustrated by the numerical example